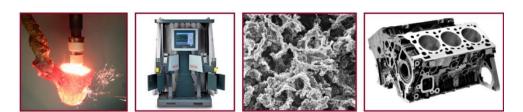


Compacted Graphite Iron – A New Material for Highly Stressed Cylinder Blocks and Cylinder Heads



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Vermicular-Graphit-Guss: Ein neues Material für höchst beanspruchte Motorblöcke und Zylinderköpfe

Dr Steve Dawson, SinterCast Ltd, London Prof. Fritz Indra, Honorary Professor, Vienna University of Technology

Abstract

The demands for downsizing and power-up continue to pose challenges for engine designers and for the materials they choose. The present state-of-the-art for highly charged diesel engine performance is 60-65 kW/litre and 150 Nm/litre. This is forecast to rise to 80 kW/litre and 200 Nm/litre in the next generation of DI diesel engines and will surely reach 100 kW/litre during the next decade. These performance demands will result in significant increases in thermal and mechanical loading and will require new material solutions.

The application of Compacted Graphite Iron (CGI) provides approximately double the fatigue limit of conventional grey iron and aluminium alloys and therefore satisfies bottom- end durability requirements without increasing the size or weight of the main bearing region. The strength and stiffness of CGI also improve the dimensional stability of the cylinder bore to reduce piston slap, bore wear, oil consumption and blow-by. The present paper provides a review of CGI material properties, engine results and comparisons to grey iron and aluminium to show how CGI can contribute to future performance, refinement and emissions objectives.

Zusammenfassung

Die Entwicklung zu immer mehr Leistung sowie die Verkleinerung der Verbrennungskraftmaschinen ist eine besondere Herausforderung für die Entwicklungsingenieure, sowie das Material das dabei verwendet werden sollte. Zurzeit haben hoch-aufgeladene Diesel-Motoren eine Literleistung von 60-65 kW sowie ein Literdrehmoment von 200 Nm.

Es ist abzusehen, dass die nächste Generation der Diesel-Motoren bis zu 80 kW/Liter sowie 200 Nm/Liter erreichen werden. In fernerer Zukunft sollten sogar 100 kW/Liter möglich sein. Die dabei sehr hohen thermischen und mechanischen Beanspruchungen erfordern neue Lösungen auf der Materialseite.

Bei der Verwendung von Vermicular-Graphit-Guss (CGI) kann mit doppelt so hohen Beanspruchungen gerechnet werden wie bei normalem Grauguss, oder Aluminium Legierungen. So können mit CGI alle Anforderungen modernster Diesel-Motoren erfüllt werden, ohne dass dabei die Größe oder das Gewicht zunehmen muss.

Die Festigkeit und Steifigkeit von CGI verbessert auch die Stabilität der Zylinderbohrung und führt so zu weniger Kolbenverschleiß und Kolbengeräuschen, reduzierter Reibleistung, verringertem Ölverbrauch und weniger blow-by Gasen.

Dieser Vortrag erklärt die Material-Eigenschaften von CGI und zeigt Ergebnissen im Vergleich zu Motoren aus Grauguss und Aluminium und macht klar wie CGI den zukünftigen Leistungs-Anforderungen von höchstbeanspruchten Verbrennungskraftmaschinen genügen kann.



Introduction

Although Compacted (vermicular) Graphite Iron was first observed in 1948, the narrow range for stable foundry production precluded the high volume application of CGI to complex components such as cylinder blocks and heads until advanced process control technologies became available. This, in turn, had to await the advent of modern measurement electronics and computer processors. Following the development of foundry techniques and manufacturing solutions throughout the 1990's, the first series production of CGI cylinder blocks began during 1999. Today, more than 40,000 CGI cylinder blocks are produced each month for OEMs including Audi, DAF, Ford, Hyundai, MAN, Mercedes, PSA and Volkswagen.

Emissions legislation and the demand for higher specific performance from smaller engine packages continue to drive the development of diesel engine technology. While higher peak firing pressures provide improved combustion, performance and refinement, the resulting increases in thermal and mechanical loads require new design solutions. Design engineers must choose between increasing the section size and weight of conventional grey iron and aluminium components or adopting a stronger material, specifically, CGI.

Given that new engine programs are typically intended to support three to four vehicle generations, the chosen engine materials not only need to satisfy current design criteria but must also provide the potential to satisfy future emissions and performance objectives, without changing the overall block architecture. With at least 75% increase in ultimate tensile strength, 40% increase in elastic modulus and approximately double the fatigue strength of either grey iron and aluminium, CGI is ideally suited to meet the current and future requirements of engine design and performance.

Microstructure and Properties

As shown in Figure 1 (a), the graphite phase in Compacted Graphite Iron appears as individual 'wormshaped' or vermicular particles. The particles are elongated and randomly oriented as in grey iron, however they are shorter and thicker, and have rounded edges. While the compacted graphite particles appear worm-shaped when viewed in two dimensions, deep-etched scanning electron micrographs (Figure 1 (b)) show that the individual 'worms' are connected to their nearest neighbours within the eutectic cell. The complex coral-like graphite morphology, together with the rounded edges and irregular bumpy surfaces of the compacted graphite particles, results in stronger adhesion between the graphite and the iron matrix, inhibiting crack initiation and providing superior mechanical properties.



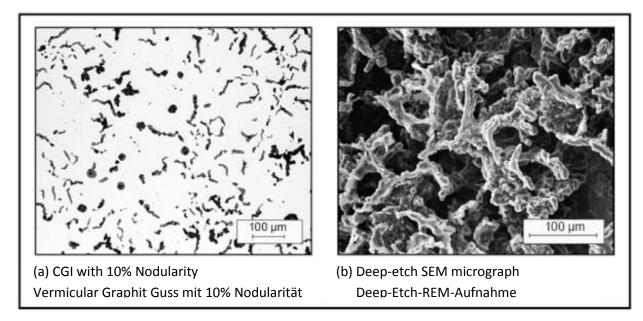


Figure 1: The vermicular graphite particles in CGI are connected to their nearest neighbours in coral-like clusters.

Die Vermiculargraphit-Partikel in CGI sind mit ihren nächsten Nachbarn in korallen-artigen Clustern verbunden.

Compacted Graphite Iron invariably includes some nodular (spheroidal) graphite particles. As the nodularity increases, the strength and stiffness also increase, but only at the expense of castability, machinability and thermal conductivity. The microstructure specification must therefore be chosen depending on both the production requirements and the performance conditions of the product. For example, the production of CGI exhaust manifolds is typically specified with up to 50% nodularity. For manifolds, the higher nodularity provides increased strength to facilitate supporting the exhaust system and also increases the flow of exhaust heat into the catalyst to achieve early light-off. In this case, the higher nodularity benefits the product without increasing the incidence of casting defects or impairing machinability.

However, in the case of cylinder blocks and heads, where castability, machinability and heat transfer are all of paramount importance, it is necessary to impose a more narrow specification. A typical specification for a CGI cylinder block or head can be summarised as follows:

- 0-20% nodularity, for optimal castability, machinability and heat transfer
- No free flake graphite, flake type graphite (as in grey iron) causes local weakness
- >90% pearlite, to provide high strength and consistent properties
- <0.02% titanium, for optimal machinability

This general specification will result in a minimum tensile strength of 450 MPa in a 25 mm diameter test bar, and will satisfy the ISO 16112 Compacted Graphite Iron standard for Grade GJV 450. The typical mechanical properties for this CGI Grade, in comparison to conventional grey cast iron and aluminium are summarised in Table I:



Table I:

Mechanical and Physical Properties of CGI in comparison to conventional grey cast iron and aluminium at 20°C

Material und physikalische Eigenschaften von CGI im vergleich zu konventionellem Grauguss und Aluminium bei 20°C

| Property | Units | GJV 450 | GJL 250 | GJL 300 | A 390.0 |
|----------------------------------|-------------|---------|---------|---------|---------|
| Ultimate Tensile Strength | MPa | 450 | 250 | 300 | 275 |
| Elastic Modulus | GPa | 145 | 105 | 115 | 80 |
| Elongation | % | 1-2 | 0 | 0 | 1 |
| Rotating-Bending Fatigue (20°C) | MPa | 210 | 110 | 125 | 100 |
| Rotating-Bending Fatigue (225°C) | MPa | 205 | 100 | 120 | 35 |
| Thermal Conductivity | W/m-K | 36 | 46 | 39 | 130 |
| Thermal Expansion | µm-m-K | 12 | 12 | 12 | 18 |
| Density | g/cc | 7.1 | 7.1 | 7.1 | 2.7 |
| Brinnell Hardness | BHN 10-3000 | 215-255 | 190-225 | 215-255 | 110-150 |

Series Production References

The successful development of CGI production and manufacturing technologies has resulted in series production programs in Europe, Asia and the Americas. A summary of publicly announced CGI programs is provided in Table II:

Table II: CGI Series Production Programs Verwendung von CGI bei heutigen Verbrennungskraftmaschinen

| OEM | Engine Details | CGI Component |
|----------------|--|-----------------------------|
| Audi | 2.7, 3.0, 4.2 & 6.0 L Passenger Vehicle Diesel Engines | V6 and V8 Cylinder Blocks |
| Caterpillar | Commercial Vehicle Engines | Cylinder Liners |
| Chrysler Group | 3.0L V6 Passenger Vehicle Engine | Cylinder Block and Bedplate |
| DAF | 12.6 L I-6 Commercial Vehicle Engine | Cylinder Block |
| DAF | 12.9 L I-6 Commercial Vehicle Engine | Cylinder Block & Head |
| Daimler | 9, 12 and 14 L Commercial Vehicle Engines | Cylinder Heads |
| Ford-PSA | 2.7 L Passenger Vehicle Diesel Engine | V6 Cylinder Block |
| Ford | 3.0, 3.6, 4.4 & 6.7 L Passenger Vehicle Diesel Engines | V6 and V8 Cylinder Blocks |
| Ford | 7.3 & 9.0 L Commercial Vehicle Engines | Cylinder Blocks and Heads |
| Hyundai | 3.0 L V6 Passenger Vehicle Diesel Engine | V6 Cylinder Block |
| Hyundai | 3.9 & 5.9 L Commercial Vehicle Engines | In-line Cylinder Blocks |
| Hyundai | 5.9, 9.9 & 11 L Commercial Vehicle Engines | Cylinder Heads |
| MAN | 10.5 & 12.4 L Commercial Vehicle Engines | Cylinder Block |
| Navistar | 6.4, 10.5 & 12.6 L Commercial Vehicle Engines | Cylinder Blocks |
| Scania | 16.4L Commercial Vehicle Engine | V8 Cylinder Block |

The current production volume equates to approximately 500,000 CGI engines per year. Although the current production is limited to diesel engines, and primarily based in Europe, several new programs have been approved and CGI production will expand to other components and other geographical regions. Specific examples include commercial vehicle cylinder heads and V-diesel cylinder blocks for North American SUV and pick-up applications. In consideration of the approved production activities, it is estimated that more than 30 different engine designs, accounting for over two million engines, will be produced during 2010 with either a CGI cylinder block or a CGI cylinder head.



Engine Design Opportunities

Relative to conventional grey cast iron, CGI provides opportunities for:

- Reduced wall thicknesses at current operating loads
- Increased operating loads at current design
- Reduced safety factors due to less variation in as-cast properties
- Reduced cylinder bore distortion
- Improved NVH
- · Shorter thread engagement depth and therefore shorter bolts

During the initial development period in the mid-1990's, much of the CGI development activity was focused on weight reduction. The data in Table III provide a summary of weight reduction results obtained in design studies conducted by various foundries and OEMs. The percent weight reduction values in parentheses refer to CGI cylinder blocks that are currently in series production and were published by the OEM. Although these cylinder blocks were never produced in grey iron (weight therefore presented as "xx.x"), the OEM stated that extra mass would have been required to satisfy durability requirements if the blocks were produced in conventional grey iron. While comparisons of the weight reduction potential depend on the size and weight of the original block, the data presented in Table III indicate that a weight reduction of 10-15% is a reasonable target for any CGI conversion program.

| Table III: |
|--|
| Weight reduction results for CGI vs. grey iron cylinder blocks |
| Gewichtsreduzierung durch CGI gegenüber Grauguss-Motorblöcken |

| Engine Size (Litres) | Engine Type | Grey Weight (kg) | CGI Weight (kg) | Percent Weight Reduction |
|-------------------------|----------------|---------------------|--------------------|-----------------------------|
| 1.6 | I-4 Petrol | 35.4 | 25.0 | 29.4 |
| 1.8 | I-4 Diesel | 38.0 | 29.5 | 22.4 |
| 2.0 | I-4 Petrol | 31.8 | 26.6 | 16.4 |
| 2.5 | V-6 (Racing) | 56.5 | 45.0 | 20.4 |
| 2.7 | V-6 Diesel | XX.X | OEM Confidential | (15) |
| 3.3 | V-8 Diesel | XX.X | OEM Confidential | (10) |
| 3.8 | V-8 Diesel | XX.X | OEM Confidential | (20) |
| 4.0 | V-8 Diesel | XX.X | OEM Confidential | (15) |
| 4.2 | V-8 Diesel | XX.X | OEM Confidential | (20) |
| 4.6 | V-8 Petrol | 72.7 | 59.6 | 18.0 |
| 9.2 | I-6 Diesel | 158 | 140 | 11.4 |
| 12.0 | V-6 Diesel | 240 | 215 | 10.4 |
| 14.6 | V-8 Diesel | 408 | 352 | 14.2 |

Since the introduction of common rail fuel injection, the emphasis in CGI engine development has shifted from weight reduction toward downsizing and increased power density. In this regard, the doubling of fatigue strength relative to grey iron and aluminium allow for significant increases in engine loading. One specific OEM study has shown that a 1.3 litre CGI engine package can provide the same performance as a current 1.8 litre grey iron engine. To achieve this increase, the P_{max} was increased by 30% while the cylinder block weight was decreased by 22%. Despite the increase in P_{max} , test rig fatigue analyses showed that the weight-reduced CGI cylinder block provided a larger safety margin that the original grey iron block, thus indicating that further increases in performance were possible. In comparison to the original engine, the fully assembled CGI engine was 5% lower, 5% narrower, 13% shorter and 9.4% lighter. This example demonstrates the contribution of CGI to achieve combined downsizing and power-up objectives.



Another consideration of CGI engine design is the ability to withstand cylinder bore distortion. In the combined presence of elevated temperatures and increased combustion pressures, cylinder bores tend to expand elastically. However, the increased strength and stiffness of CGI is better able to withstand these forces and maintain the original bore size and shape. Table IV shows comparative bore distortion results for four grey iron and CGI engines with the same design.

| Engine Size (Litres) | Engine Type | % Improvement CGI vs Grey |
|-------------------------|----------------|------------------------------|
| 1.8 | I-4 Petrol | 18 |
| 1.8 | I-4 Diesel | 20 |
| 2.2 | I-4 Petrol | 28 |
| 4.6 | V-8 Petrol | 22 |

Table IV: Cylinder bore distortion for CGI vs grey iron Reduzierter Zylinderverzug bei Verwendung von CGI gegenüber Grauguss

The improved cylinder bore distortion allows for reduced ring tension and thus reduced friction losses. The improved bore-ring matching also provides a series of secondary contributions including reduced piston slap thus improving NVH; reduced oil consumption thus extending oil change intervals; and, reduced blow-by thus preventing torque loss and improving emissions. From the design perspective, these results indicate the potential to reduce the thickness of the cylinder bore walls to provide further weight and thermal benefits.

The increased stiffness of CGI also contributes to NVH performance. Although the specific damping capacity of CGI is lower than that of grey iron, the higher elastic modulus effectively stiffens the block, making many webs and ribs redundant. As the vibration frequency is proportional to the square root of the stiffness, the 40% increase in the elastic modulus of CGI causes a positive shift in the Eigenfrequency spectrum which, in turn, increases the separation between the combustion firing frequency and the resonant frequencies of the block. The net result of this increased separation is that the engine operation becomes quieter. The positive shift in the first torsional frequency mode and the reduced noise level of several CGI engines tested in semi-anechoic chambers are shown in Table V, both for passenger vehicle and commercial vehicle engines.

| Table | V: |
|-------|----|
|-------|----|

NVH results for identically designed CGI and grey iron engines Geräuschverbesserungen bei Verwendung von CGI gegenüber Grauguss

| Engine Size (Litres) | Engine Type | First Torsional Frequency Shift | Sound Pressure Level (dBA) |
|-------------------------|----------------|------------------------------------|-------------------------------|
| 1.8 | I-4 Diesel | +12% | Same |
| 2.0 | I-4 Petrol | +8% | -1.0 to -1.5 |
| 2.0 | I-4 Petrol | +7% | -1.0 to -1.5 |
| 2.2 | I-4 Petrol | +16% | -1.0 to -1.5 |
| 2.4 | I-4 Diesel | +9% | -1.0 to -1.5 |
| 4.6 | V-8 Petrol | +12% | Not Tested |
| 5.8 | V-8 Petrol | +18% | Not Tested |
| 12.0 | V-6 Diesel | +8% | -0.5 to -1.0 |
| 13.8 | I-6 Diesel | +8% | Not Tested |



CGI vs. Alloyed Grey Iron

As the increases in engine loading began to exceed the strength capabilities of conventional grey iron (GJL 25), foundries and OEMs responded by adding alloying elements and hardening agents such as Chromium, Nickel, Copper, Tin and Molybdenum to increase the tensile strength. In order to further increase the strength to fully satisfy the 300 MPa minimum tensile strength objective (GJL 30), some specifications also reduced the carbon content from approximately 3.2% to 3.0% to make the graphite flakes smaller, thus reducing the risk for crack initiation and propagation. While the alloying and reduced carbon content provide a 10-20% increase in mechanical properties, these actions simultaneously consume many of the core advantages of conventional grey cast iron: castability, heat transfer, machinability and significantly, cost.

Castability: During solidification, the formation of graphite flakes in conventional grey iron provides an expansion effect that counteracts the natural shrinkage tendency of the iron. However, the lower carbon content of alloyed grey iron reduces the extent of this beneficial effect. Additionally, many of the alloying elements (Cr, Cu, Sn, Mo) segregate to the last areas of the casting to solidify increasing the sensitivity for shrinkage porosity and carbide formation. The net effect is that the castability of alloyed grey iron, including feeding requirements, is effectively the same as that of CGI. This is particularly true for complex castings such as 4-valve cylinder heads.

Heat Transfer: The addition of alloying elements to grey iron reduces thermal conductivity. Typical alloying levels for GJL 30 (0.3% Cr and 0.3% Mo) reduce the thermal conductivity of grey iron by 10-15%. Further, since grey iron relies on the elongated graphite flakes to provide natural conduits for heat transfer, the lower carbon content of alloyed grey iron also detracts from the heat transfer capability. The net effect is that the thermal conductivity of alloyed grey iron is only about 5-7% higher than that of a standard pearlitic CGI.

Machinability: The alloying elements added to increase the strength of grey iron also increase the hardness and wear resistance. While the strength of alloyed grey iron is only 10-20% higher than that of conventional grey iron, the hardness can be 30% higher. Depending on the alloy content, the hardness of alloyed grey iron can frequently be higher than that of CGI (Table I). While there is indeed a significant difference in machinability between conventional grey iron and CGI, the tool life for alloyed grey iron and CGI are effectively the same for many machining operations.

Cost: The shrinkage sensitivity (feeding requirements) and machinability (tool life) of alloyed grey iron both impact the total on-cost of alloyed grey iron compared to normal grey iron (GJL 25). Beyond these operational concerns, consideration must also be given to the cost of the alloying elements. For example, the market price of molybdenum has increased from approximately EUR 5,000 per tonne to EUR 50,000 per tonne since 2004. For a 100 kg casting with a 70% mould yield and a 0.3% Mo content, the molybdenum cost alone is approximately EUR 20 per casting.

NVH: The primary property for the determination of NVH performance is stiffness. While the increase from GJL 25 to GJL 30 provides a 20% increase in tensile strength, the increase in elastic modulus is only about 10%. In comparison, CGI provides a 40% increase in modulus compared to GJL 25. Despite that the specific damping capacity of CGI is lower than that of either of the two grey iron Grades, the increased stiffness of CGI typically results in a reduced noise level of approximately 1.0 dB.



In hindsight, alloyed grey iron was indeed the right material choice for heavily loaded cylinder blocks and heads in 1999, before CGI was proven as a viable high volume material. However, the recent advances in CGI foundry process control and manufacturing technology have established CGI as a proven series production material. As a result, it is no longer necessary to accept the trade-offs associated with alloyed grey iron. Alloyed grey iron brings many of the same challenges as CGI with respect to castability, heat transfer, machinability and cost, but not the benefits. If designers are willing to incur the operational penalties of alloyed grey iron, they should instead specify CGI to realise the full increase in material properties and to realise the full benefits related to engine performance, NVH and durability.

CGI vs. Aluminium

In comparison to aluminium, the mechanical properties of CGI provide opportunities for:

- Smaller package size
- Higher specific performance
- Reduced cylinder bore distortion and improved oil consumption
- No cylinder liners or surface etchant/coating
- Improved NVH
- Lower production cost
- Improved recyclability

Due to the considerable density difference between CGI (7.1 g/cc) and aluminium (2.7 g/cc), it is to be expected that a CGI cylinder block will be heavier than a similar displacement aluminium block. However, because of the higher strength and stiffness of CGI, the main bearing thickness (and in V-engines the cylinder bank off-set angle) can be reduced to provide a significantly shorter cylinder block. Accordingly, all of the components that span the length of the cylinder block – such as the cylinder heads, crankshaft, camshaft and bedplate – can also be made shorter, and thus lighter. This is particularly advantageous in V-blocks with two cylinder banks. The net result is that a fully assembled CGI engine can indeed have the same weight as a fully assembled aluminium engine. This result is evident from Table VI which shows that the Audi 4.2 litre V8 TDI based on a CGI cylinder block is actually 4 kg smaller and lighter than the Mercedes 4.0 litre V8 CDI aluminium engine.

| T | able | VI: |
|---|------|-----|
| | | |

The Audi 4.2 litre CGI V8 is 4 kg smaller and lighter than the Mercedes 4.0 litre aluminium V8 Der Audi 4.2 Ltr. CGI V8 ist 4 kg leichter und kleiner als der Mercedes 4.0 Ltr. Aluminium V8

| Parameter | Audi 4.2 V8 TDI | Mercedes V8 CDI |
|---------------------------------|-----------------|-----------------|
| Performance (kW) | 240 | 231 |
| Specific performance (kW/litre) | 57 | 57 |
| Torque (Nm @ rpm) | 650 @ 1600 | 580 @ 1600 |
| Acceleration (0-100 km/hr, sec) | 5.9 | 6.1 |
| Bore pitch (mm) | 90 | 97 |
| Overall length (mm) | 520 | 640 |
| Engine weight (kg) | 255 | 259 |
| Power-to-weight (kW/kg) | 0.94 | 0.89 |



Even within the in-line sector, it can be shown that the energy intensity of iron vs. aluminium production results in a significant energy penalty for aluminium. With current recycling rates, each tonne of cast iron (grey, CGI or ductile) accounts for an equivalent energy content of approximately 10,500 MJ/tonne. The corresponding value for aluminium is approximately 90,000 MJ/tonne. Assuming that a CGI cylinder block weighs 35 kg and the corresponding aluminium cylinder block weighs 28 kg, the net energy penalty to society for the aluminium block is approximately 2,150 MJ/block.

Given an energy content of 34 MJ/litre for gasoline, the as-cast energy penalty of 2,150 MJ corresponds to approximately 63 litres of gasoline. Further, assuming standard estimates of 0.5 litres of petrol saved for each 100 km and each 100 kg of weight saving, the 7 kg weight reduction provided by the aluminium block over the CGI block would require a driving distance of approximately 180,000 km to payback the energy differential. At average European driving distances of 15,000 km per year, this corresponds to approximately 12 years of driving – longer than the operating life of the average European passenger vehicle. It is thus evident that factors such as mechanical properties and cost are not the only considerations in favour of CGI over aluminium. OEMs must also consider the cradle-to-grave energy balance for society, particularly in developing countries where the planned economics place added value on energy dependence.

Design Considerations

All CGI cylinder blocks for passenger car applications are produced with a minimum wall thickness of 3.5 mm (-0.5, +1.0). This is the same as for conventional grey cast iron and confirms that CGI has sufficient fluidity to fill complex state-of-the-art moulds. Given that the minimum wall thickness for CGI is the same as for grey iron (dictated by sand moulding considerations) the weight reduction opportunity is not based on minimum-wall thickness capabilities. Rather, the weight reduction opportunity for CGI cylinder blocks is based on re-designing the relatively thick load-bearing walls of the casting. For example, the reduction of a main bearing wall from 20 mm to 15 mm provides a significant weight reduction, without infringing on foundry process capability. In contrast, a reduction of the water jacket from 3.5 mm to 3.0 mm may exceed process capability and yet only provide a small weight reduction. The higher strength of CGI allows designers to reduce weight by focusing on the relatively thick load-carrying regions of a casting that are not yet limited by moulding considerations. Although every kilogram is important in a casting, and thick and thin sections must both be addressed, the most effective contributions to weight reduction are those made to the thick sections, as enabled by the improved mechanical properties of CGI.

When specifying grey or ductile iron, design engineers know that uniform graphite shape is critical to maintaining mechanical properties. In grey iron, the presence of degenerate graphite forms such as undesirable D-Type graphite result in a 20-25% reduction in mechanical properties. Similarly, 'crab-shaped' graphite or exploded nodules reduce the strength and stiffness of ductile iron. Based on these experiences, designers may be inclined to specify a uniform graphite structure in CGI. However, while 0-20% nodularity structures are required in performance-critical sections to optimise castability, thermal conductivity and machinability, higher nodularities can actually benefit the outer structural regions of a casting. The natural tendency of CGI to solidify with higher nodularity in the faster cooling sections may result in the thin outer walls (less than ~5 mm) having up to 50% nodularity. Where the thin sections are not thermally loaded and do not require extensive machining, the higher nodularity only serves to increase the strength, stiffness and ductility of the castings. CGI microstructure specifications should therefore focus on performance-critical sections such as the cylinder bore walls and main bearings and, whenever possible, take advantage of the increased nodularity in thin wall areas.



Thermal fatigue failures in grey iron are often rectified by adding material to reinforce strength and stiffness. However, the lower thermal conductivity of CGI causes thermally loaded CGI components to operate at higher temperatures. Therefore, if a CGI component experiences thermal fatigue, particularly in material substitution applications based on existing grey iron designs, the solution may lie in reducing - not increasing - wall thicknesses to improve heat transfer. It is also important to optimise the design of the cooling water channels to ensure that the cooling water is introduced as close as possible to the heat source to maximise the cooling efficiency. Because of the higher elastic modulus and lower thermal conductivity of CGI relative to grey iron, it is clear that the thermal stress loading in a similarly designed CGI component will be higher than that in the grey iron component. Ultimately, the ability for CGI to provide improved durability requires that the strength increase is greater than the increase in thermal load, thus providing a net benefit. In some cases, this will require an improved design of the water channel.

Another consideration related to thermal loading is that many bench tests for heavy-duty cylinder heads rely on severe thermal cycles to minimise the test duration. However, rapid heating and cooling rates favour materials with high thermal conductivity (in contrast, higher absolute temperatures and longer holding times favour materials with higher mechanical strength). Therefore, the design of many bench scale thermal fatigue tests favour grey iron while the actual in-service duty-cycle would favour CGI. Re-designed CGI components have confirmed this premise. Care must therefore be taken to ensure that short-duration bench tests do not wrongly condemn a CGI component.

Standards and Terminology

Several national and international organisations have developed and published standards for CGI. These standards specify the CGI Grades in terms of the tensile strength and the microstructure, expressed as percent nodularity. The currently available standards are summarised in Table VII.

| Country | Issuing Body | Number | Year |
|---------------|--------------|-----------|------|
| International | ISO | ISO 16112 | 2006 |
| International | SAE | J 1887 | 2002 |
| Germany | VDG | W 50 | 2002 |
| USA | ASTM | A 842-85 | 1997 |
| China | JB | 4403-87 | 1987 |
| China | GB/T | 26655 | 2011 |
| Romania | STAS | 12443-86 | 1986 |

Table VII: Summary of CGI Standards Zusammenfassung der CGI Normen

Historically, CGI has been known by the names "Compacted Graphite Iron" and "Vermicular Graphite Cast Iron", with the "compacted" terminology primarily being used in English speaking countries and the "vermicular" terminology predominating in most other languages. Most recently, during 2006, the new ISO standard for CGI was published using the combined name: "Compacted (Vermicular) Graphite Cast Iron". The ISO designation for CGI has been abbreviated as "GJV" and five Grades have been specified based on the minimum ultimate tensile strength obtained in separately cast test pieces, including: GJV 300 (ferritic), GJV 350, GJV 400, GJV 450 (pearlitic) and GJV 500 (alloyed). CGI is now formally recognised by many of the leading standardisation bodies related to the international automotive and foundry industries including the ISO, SAE, VDG and ASTM. In 2011, China published a new standard for CGI which specifies a 0-20% nodularity range. The older JB 4403-87 standard, which allowed a 0-50% nodularity range remains for components with simple geometries and limited thermal and mechanical loading. However, the new GB/T 26655-2011 standard applies for complex components such as cylinder blocks and heads, thus aligning China with the other standards.



Beyond the standards issued by the national and international organisations, several OEMs have also established their own internal CGI Specifications, including: Audi, BMW, Caterpillar, Cummins, DAF Trucks, DaimlerChrysler, Ford, General Electric, General Motors, Hyundai, John Deere, Opel, Rolls Royce Power Engineering and Volkswagen, among others.

Conclusion

The improved mechanical properties of Compacted Graphite Iron relative to grey iron and aluminium provide many contributions to the design and performance of internal combustion engines for passenger and commercial vehicles. Since 1999, series production experience has established CGI as a viable high volume engine material. Perhaps the most compelling statistic regarding CGI cylinder blocks is that no OEM has only one CGI cylinder block in its line-up. Without exception, every OEM that has launched the production of a CGI engine has also proceeded to develop, approve or launch additional CGI engines.



Head Office

SinterCast Ltd Kingswick House Kingswick Drive Sunninghill Berkshire SL5 7BH United Kingdom Tel: +46 150 794 40

Technical Centre

SinterCast AB (publ) Kungsgatan 2 641 30 Katrineholm Sweden Tel: +46 150 794 40

USA

SinterCast Inc 1755 Park Street Suite 200 Naperville IL 60563 USA Tel: +1 630 778 3466

China

SinterCast Trading (Beijing) Co., Ltd Room 1131, 11/F, Block A, Gateway No. 18 Xiaguangli North Road East Third Ring Chaoyang District, Beijing China, 100027 Tel: +86 10 5923 1163

Korea

SinterCast Korea Co., Ltd Rosavallcity No. 310 HyoJa-Ro 194, WanSan-Gu Jeon Ju City, 560-900 South Korea Tel: +82 10 9228 1764



www.sintercast.com info@sintercast.com

